

## The Application of Load Curve Segment Technology in Dynamic Reactive Power Optimization of Distribution Network

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**Abstract:** Dynamic reactive power optimization is about the continuous variation of the load, and considers the problem of the optimization of the motion numbers of reactive power compensation equipment action. Set up the objective function and constraint conditions in the process of dynamic optimization, and divide the load curve into segments. The objective function is the minimum of network loss and compensation capacity in the limit of the voltage, and the constraints includes the maximum numbers of compensation equipments and so on. In addition, the paper improves the segmentation technology on the basis of further researching the advantages and disadvantages of the existing load curve segmentation methods. Normalize the reactive load in the whole day and compare the difference of average and original data with threshold value for segmentation again. Apply the improved segmentation method and the multi-agent ant colony algorithm which are put forward in this paper to dynamic reactive power optimization in distribution network. The experimental results verify the effectiveness of this method.

**Keywords:** power system; dynamic reactive power optimization; load segmentation technology; intelligent algorithm

### I. INTRODUCTION

In the field of power system, reactive power optimization is a hot issue. Consider the load which varies with time, on a particular moment, fixed load of static reactive power optimization cannot meet the demand of practical engineering. So the dynamic reactive power optimization can be wide application and all-round development. Realizing the dynamic reactive power optimization needs to make load curve transform into discrete curves, namely the load curve is segmented according to certain strategy. In this way, too complicated dynamic reactive power optimization problems can turn into a number of interrelated periods of static reactive power optimization problems, and simplify the space-time coupling problems.

### II. THE MATHEMATICAL MODEL OF REACTIVE POWER OPTIMIZATION

The mathematical mode of reactive power optimization is composed of the objective function and constraint conditions. The objective function needs to consider various factors, such as the minimum loss of system network; the minimum investment of total net; the maximum number of reactive power compensation equipment action allows at least<sup>[1]</sup>.

The objective function is the minimum of network loss and compensation capacity in the limit of the voltage, the following formulas:

$$\min F = \min \left[ \alpha P_{loss}(t) + \beta \sum_{i=1}^n \left( \frac{\Delta U}{U_{i \max} - U_{i \min}} \right)^2 + \gamma \sum_{i=1}^m Q_{ci} \right] \quad (1)$$

$$P_{loss}(t) = \sum_{i \in S_G} P_{Gi}(t) - \sum_{i \in S_B} P_{Di}(t) \quad t = 1, 2, \dots, T \quad (2)$$

$$\Delta U = \begin{cases} U_i - U_{i \max} & ; & (U_i > U_{i \max}) \\ 0 & ; & (U_{i \min} \leq U_i \leq U_{i \max}) \\ U_{i \min} - U_i & ; & (U_i < U_{i \min}) \end{cases} \quad (3)$$

In these formulas:  $P_{loss}(t)$  means the active loss of line;  $U_{i \max}$  and  $U_{i \min}$  are respectively the upper and lower limits on the line of node voltage allows;  $Q_{ci}$  is reactive compensation capacity of the first i node;  $\alpha, \beta, \gamma$

shows respectively the weighted coefficient of active network loss, the limit coefficient of node voltage, the capacity coefficient of reactive power compensation;  $P_{Gi}(t)$  is active power of the first  $i$  generator at  $t$  time;  $P_{Di}(t)$  is active load of the first  $i$  node at  $t$  time.

Equality constraint conditions:

$$\begin{cases} P_{Gi} - P_{Di} - U_i \sum_{j \in S_B} U_j (G_{ij} \cos \delta_{ij} + B_{ij} \sin \delta_{ij}) = 0 \\ Q_{Gi} - Q_{Di} - U_i \sum_{j \in S_B} U_j (G_{ij} \sin \delta_{ij} - B_{ij} \cos \delta_{ij}) = 0 \end{cases} \quad (i \in S_B) \quad (4)$$

In these formulas:  $P_{Gi}(t)$ ,  $Q_{Gi}(t)$  is active power and reactive power of the first  $i$  generator at  $t$  time;  $P_{Di}(t)$ ,  $Q_{Di}(t)$  shows active load and reactive load of the first  $i$  node at  $t$  time.  $S_B$  is the total number of nodes in the system;  $U_i$ ,  $U_j$  represents voltage amplitude of the node  $i$ ,  $j$ ;  $\delta_i$ ,  $\delta_j$  shows phase Angle of the node  $i$ ,  $j$ ;  $\delta_{ij}$  is phase Angle difference between the node  $i$  and  $j$ ;  $G_{ij}$ ,  $B_{ij}$  is respectively system node admittance matrix of the first  $i$  row first  $j$  column element in the real part and imaginary part.

Inequality constraints include the generator reactive power output, the compensation device of reactive power compensation capacity, the variable ratio of on-load voltage regulating transformer, the action number constraints of two types of equipment ,load node voltage, they are shown in the following formulas:

$$Q_{Gi \min} \leq Q_{Gi} \leq Q_{Gi \max} \quad (5)$$

$$Q_{Ci \min} \leq Q_{Ci} \leq Q_{Ci \max} \quad (6)$$

$$T_{i \min} \leq T_i \leq T_{i \max} \quad (7)$$

$$u_{i \min} \leq u_i \leq u_{i \max} \quad (8)$$

In these formulas,  $Q_{Gi}$  is the reactive power generator of the node  $i$ ,  $Q_{Gi \max}$ ,  $Q_{Gi \min}$  shows the upper and lower limits for the reactive power generator of the node  $i$ ;  $Q_{Ci}$  is reactive power compensation capacity of the first  $i$  reactive compensation devices,  $Q_{Ci \max}$ ,  $Q_{Ci \min}$  shows the upper and lower limits on the capacity of the first  $i$  reactive power compensation devices;  $u_i$  is voltage of the node  $i$ ,  $u_{i \max}$ ,  $u_{i \min}$  means the upper and lower limits for voltage of the node  $j$ ;  $T_i$  is variable ratio of the first  $i$  on-load voltage regulating transformer,  $T_{i \max}$ ,  $T_{i \min}$  shows the upper and lower limits for the variable ratio of the first  $i$  on-load voltage regulating transformer.

According to inequality constraints of the dynamic reactive power optimization, as shown below:

$$\sum_{t=0}^T |C_{m,t+1} \oplus C_{m,t}| \leq C_{\max} \quad (9)$$

$$\sum_{t=0}^T |T_{l,t+1} \oplus T_{l,t}| \leq T_{\max} \quad (10)$$

In these formulas,  $T$  is a total number of segments;  $C_{m,t}$  means the switching state of the first  $m$  capacitor at  $t$  time, 0, 1 shows respectively the opening and closing;  $C_{\max}$  is the allowed maximum number of capacitor switch;  $T_{l,t}$  means values of the first  $l$  on-load voltage regulating transformer tap gear ;  $T_{\max}$  shows the allowed maximum number of tap.

### III. LOAD CURVE SEGMENTATION TECHNOLOGY

There are two kinds of segmentation of methods for load curve segmentation in theory:

(1) According to 24 hours a day, the load curve is divided into 24 segments in the whole day, integral mean value is used to determine the equivalent load of each period [2].

(2) The load curve will be segmented according to monotone [3]. Start-stop time points are usually selected as curve peaks and troughs. In addition, inflection points are also used as the start-stop time points of curve section. In this paper, based on the existing segmentation methods, new ideas strike the segmentation method. Specific segmentation method is as follows:

(1) According to the related data of the load, data will be carried on the normalization, and form the normalized

load curve;

Normalize the formula is as follows:

$$y = (x - x_{\min}) / (x_{\max} - x_{\min}) \quad (11)$$

In this formula,  $y$ ,  $x$  is respectively processing data before the normalization and normalized processing of data,  $y \in [0, 1]$ ;  $x_{\min}$  and  $x_{\max}$  mean the minimum and maximum of reactive load;

(2) Calculate the reactive load average which is after the normalization of the adjacent two time stages within 24 hours:

$$Q_{\text{avt}} = \frac{Q_{t+1} + Q_t}{2} \quad t = 1, 2, \dots, 23 \quad (12)$$

In this formula,  $Q_{\text{avt}}$  shows the average of the reactive load which is between two time stages;  $Q_t$ ,  $Q_{t+1}$  refers to respectively reactive load at  $t$ ,  $t+1$  time;  $Q_{\text{avt}}$ ,  $Q_t$ ,  $Q_{t+1}$  is the normalized reactive load value.

(3) Judge  $|Q_{\text{avt}} - Q_t| \leq \varepsilon$ ,  $\varepsilon$  is the threshold value, determine the size of its value through repeated experiments.

(4) Determine the equivalent load: If the difference is greater than the threshold value, keep the initial value of the reactive load unchanged; If less than or equal to the threshold value, the average of the initial value of reactive load is used as the reactive load value at this time; If reactive load around the adjacent value at a certain time is less than the threshold, select small numerical reactive load as the new load value at this time.

#### IV. DYNAMIC REACTIVE POWER OPTIMIZATION PROCESSES

The specific process of dynamic reactive power optimization of distribution network is following:

- (1) Initialization: read the system of network data, set the initial parameters of optimization algorithm;
- (2) Segment the system of reactive power load curve : the paper uses the improved segmentation technology to segment the curve, and set the threshold in advance to get the reactive load at each time period;
- (3) The multi-agent ant colony algorithm<sup>[4]</sup> is applied in reactive power optimization, and the maximum allowable operating frequency and the active power loss value of the transformer tap and load regulating transformer tap at each time period are obtained.
- (4) Finally determine whether meet the terminative conditions according to the constraint conditions and the number of iterations, so the optimization strategy is obtained.

#### V. THE EXAMPLE ANALYSIS

Take a certain regional power distribution network with 14 nodes as an example, a numerical example is analyzed, and the wiring diagram of system is shown in Figure 1:

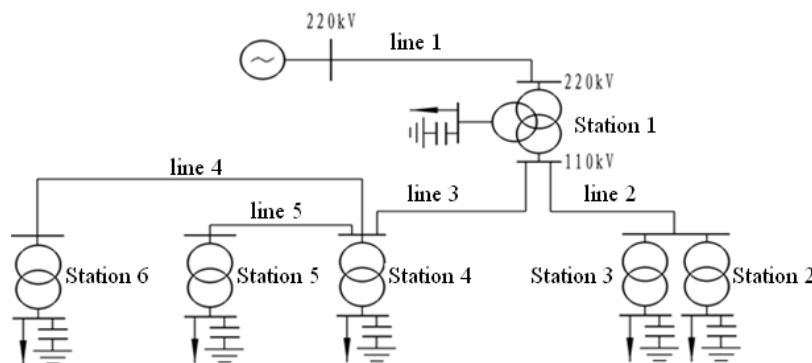


Figure1 the wiring diagram of a regional power distribution network with 14 nodes

Draw the load curve of daily variation according to the related parameters<sup>[5]</sup> of the power distribution network in the region, the result is shown in figure 2:

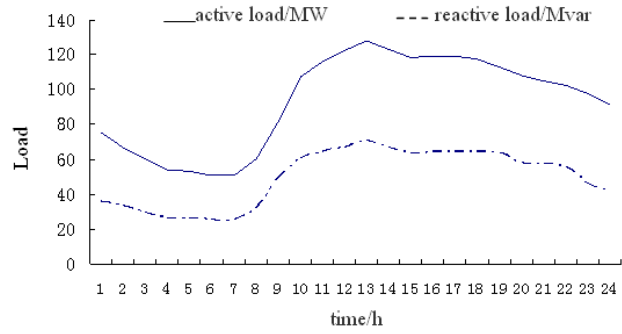


Figure2 load diurnal variation curve in the whole network

The reactive load curve is normalized according to Formula (11), the result is shown in Figure 3:

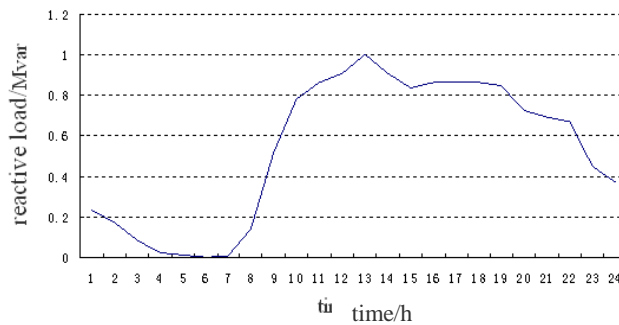


Figure3 the daily changed curve of reactive load after normalization

When the threshold is 0.01, 5 ~ 6 times, 15 ~ 18 is respectively combined into a segment, the reactive load curve is divided into 20 sections, the result is shown in figure 4; When the threshold is 0.02, 4 ~ 7 times, 15 ~ 19, 20 ~ 22, 23 ~ 24 is respectively merged into the other segment, the reactive load curve includes 14 sections in total, which is shown in figure 5. When the threshold is 0.03, 1 ~ 2 times, 3 ~ 7, 11 ~ 12, 14 ~ 18, 19 ~ 22, 23 ~ 24 is respectively combined into a segment, the reactive load curve is divided into 10 sections, which is shown in figure 6:

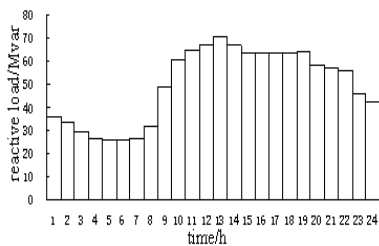


Figure 4  $\varepsilon = 0.01$

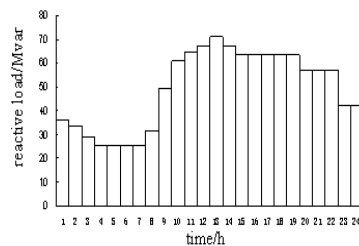


Figure 5  $\varepsilon = 0.02$

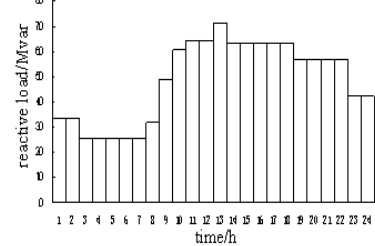


Figure 6  $\varepsilon = 0.03$

The selection of the threshold is directly related to the number of segments from figure 1.4~1.6, so the threshold is set to 0.02 through repeated experiments. With respect to  $\varepsilon = 0.01$ , the computation scale and operation time are reduced, and the operation time is saved. Compared with  $\varepsilon = 0.03$ , the result is closer to the actual load curve, meanwhile the operation precision and accuracy can be improved. Reactive power optimization of the power distribution network is carried out by using multi-agent ant colony algorithm, and the result is as follows:

When the reactive load curve are divided into different segments, the action times in each of the capacitor bank is listed on the table 1, the conversion of the N capacitor bank is n times.

Table 1 the number of the capacitor bank actions in different cases

Max action times Segments	Site1	Site2	Site3	Site4	Site5	Site6
10	4	2	4	0	2	0
14	6	4	4	2	4	2
20	6	4	4	2	4	2
Static	6	4	4	2	4	2

When the reactive load curve are divided into different segments, the number of transformer tap actions in each site is listed on the table 2, the conversion of the N transformer tap adjusting gear is n times.

Table 2 the number of transformer tap actions in different cases

Max action times Segments	Site2	Site3	Site4	Site5	Site6
10	4	4	2	4	4
14	8	6	4	8	6
20	8	6	4	8	6
Static	8	6	4	8	6

The table1~2shows:

- (1) The number of segments is 10, although the capacitors and transformer action times are less, the constraints are too harsh not to fully realize the optimization, there is still a lot of reactive power flow in the line;
- (2) When the number of segments is 14, the number of action times of the capacitors is consistent with that of the static optimization. That is to say, the input of the capacitors and the location of the transformer taps are to meet the requirements of the system.

(3) The number of amplification segment is again limited to 20 segments, the number of switching capacitors and transformer tap actions are not changed. This suggests that segmenting the load curve is not the more the better, excessive segmentation is no practical significance, and the operation time will increase greatly. When the number of segments is 14, the result is listed on the table 3. According to the Formula (9), (10) which lies in the constraint conditions, set the relationships between the maximum allowable number of different devices action, the active power loss throughout the day and the average calculating time:

Table 3 Active power loss and calculating time of dynamic reactive power optimization

Max allowable action times	Active power loss/p.u.	Time/s
5	0.1321	14.05
10	0.1173	8.96
15	0.1094	5.53
20	0.1098	5.24

From the table 3, the maximum allowable number of devices action is set to 15 to meet the actual needs. If Beyond the number of segments is too large, it is no practical significance. In addition, but also because the device moves too frequent, this case will lead to the reciprocating phenomenon of active network loss. Not only does it not reduce operation scale, but also it can add the calculating time. The experimental results show: when the threshold is set to 0.02, and the load curve is divided into 14 segments, which can meet the demand of reactive power optimization of the distribution network.

## VI. CONCLUSION

On the basis of full study of the theory of load curve segmentation, the existing methods are improved, the improved method is applied in a certain regional power distribution network system with 14 nodes, the experimental results show the improved segmentation method is practical. Compared with traditional segmentation method, on the scale of operation and operation precision is superior.

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